

Determination and Prediction of Orbital Parameters of the Radioastron Mission

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Radioastron mission

| Orbit | Mission |
|---|-----------------------------------|
| <i>Launch date:</i> 18 July 2011 | <i>Purpose:</i> VLBI observations |
| <i>Perigee altitude:</i> 1000 – 67 000 km | <i>Bands:</i> P, L, C, K |
| <i>Apogee distance:</i> up to 370 000 km | <i>Data channel:</i> 2x72 Mbps |
| <i>Period:</i> 8–9 days | |

Orbit knowledge is required for the interferometric data correlation.

Main perturbations

| Nature | Maximum, m/s ² | Average, m/s ² |
|------------------------|------------------------------|------------------------------|
| Spherical harmonics | $3.8 \cdot 10^{-3}$ | $3.3 \cdot 10^{-6}$ |
| Third bodies | $2.3 \cdot 10^{-4}$ | $4.1 \cdot 10^{-5}$ |
| Direct solar radiation | $1.9 \cdot 10^{-7}$ | $1.5 \cdot 10^{-7}$ |
| Unloadings | $5.8 \cdot 10^{-8}$ | $5.8 \cdot 10^{-8}$ |
| Tides | $6.6 \cdot 10^{-8}$ | $2.3 \cdot 10^{-11}$ |
| Earth radiation | $2.1 \cdot 10^{-8}$ | $1.1 \cdot 10^{-10}$ |

The satellite is not equipped with accelerometers.

Unloadings of reaction wheels

An unloading consists of dozens of firings, j -th firing of the i -th unloading provides $\Delta \mathbf{v}_{ij} = \frac{\Delta m_{ij} I(\tau_{ij})}{M} \mathbf{e}_{ij}$ at t_{ij}

All firings of the unloading are summed up into one impulse $\Delta \mathbf{v}_i$ applied at weighted time t_i .



Weighted time and the estimate of the impulse are as follows

$$t_i = \frac{\sum_j v_{ij} t_{ij}}{\sum_j v_{ij}} \quad \mathbf{v}_i^0 = \sum_j \mathbf{v}_{ij} (\Delta m_{ij}, \tau_{ij}, \mathbf{e}_{ij}).$$

The perturbation due to unloadings on the interval of interest is described with the set of impulses $\{\Delta \mathbf{v}_i, t_i\}$.

Direct solar radiation pressure

Decomposition of the solar radiation impacting a flat surface

$$\mathbf{F} = (1 - \alpha)\mathbf{F}_a + \alpha\mu\mathbf{F}_s + \alpha(1 - \mu)\mathbf{F}_d$$

$\alpha \in [0, 1]$ — reflectivity,

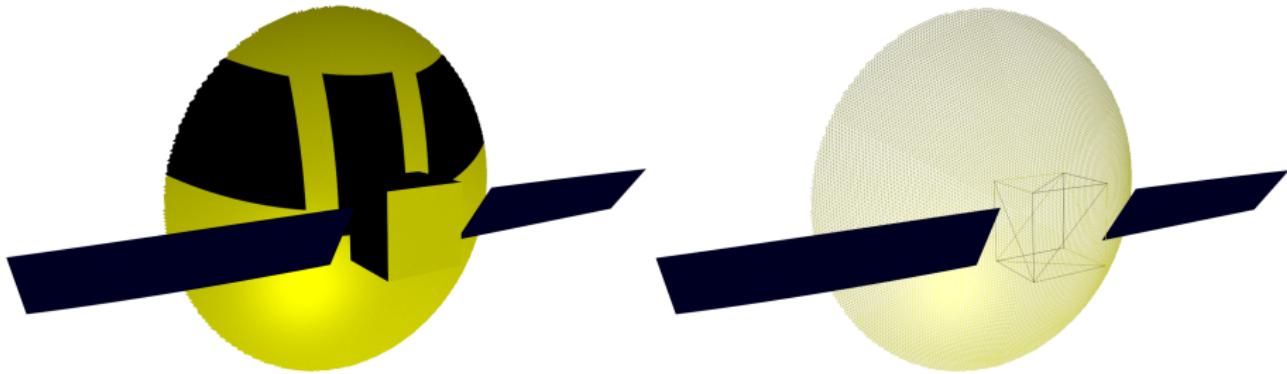
$\mu \in [0, 1]$ — specularity.

allows to represent net SRP force and torque as functions of parameters α_i and μ_i

$$\mathbf{F}_{SRP} = \sum_{i=1}^N \eta_i \mathbf{F}(A_i, \mathbf{s}, \mathbf{n}_i, \alpha_i, \mu_i),$$

$$\mathbf{M}_{SRP} = \sum_{i=1}^N \eta_i \mathbf{r}_i \times \mathbf{F}(A_i, \mathbf{s}, \mathbf{n}_i, \alpha_i, \mu_i),$$

The satellite structure



| Element | Surface | Coefficients |
|-----------------------|------------------|------------------------|
| space radio telescope | reflecting (MLI) | α_1, μ_1 |
| spacecraft bus | reflecting (MLI) | α_1, μ_1 |
| solar panels | absorbing | $\alpha_2 (\mu_2 = 1)$ |

specularity coefficient of solar panels is fixed to avoid strong correlation with α_2

Propagation

passing through an unloading:

$$(t_{i-0}, \mathbf{r}(t_{i-0}), \mathbf{v}(t_{i-0}), \dots) \rightarrow (t_{i+0}, \mathbf{r}(t_{i+0}), \mathbf{v}(t_{i-0}) + \Delta \mathbf{v}_i, \dots),$$
$$(t_{i-0}, \mathbf{r}(t_{i-0}), \mathbf{v}(t_{i+0}) - \Delta \mathbf{v}_i, \dots) \leftarrow (t_{i+0}, \mathbf{r}(t_{i+0}), \mathbf{v}(t_{i+0}), \dots).$$

| | |
|-----------------|--|
| Gravity field | EGM96 |
| Third bodies | DE-405 |
| Tides | IERS 2003 convention |
| Direct SRP | parameterized with α_1 , μ_1 and α_2 |
| Earth radiation | 18x9 constant coeff. |

Motion of the center of mass is determined by :

$$\mathbf{X}_0(t_0), \alpha_1, \mu_1, \alpha_2, \Delta \mathbf{v}_1, \dots, \Delta \mathbf{v}_n$$

Observations

Radio

- Two-way range, two-way Doppler
- One-way Doppler

| System | Band | D | \dot{D} | \dot{D}_{1w} |
|------------------------------|-------|-----|-----------|----------------|
| Ussuriysk RT-70, "Klen-D" | C | ✓ | ✓ | |
| Ussuriysk RT-70, "Phobos" | X | | | ✓ |
| Bear Lakes RT-64, "Cobalt-M" | C | ✓ | ✓ | |
| Bear Lakes RT-64, "Cortex" | X | | | ✓ |
| Puschino RT-22 | X, Ku | | | ✓ |
| Green Bank, 140ft | X, Ku | | | ✓ |

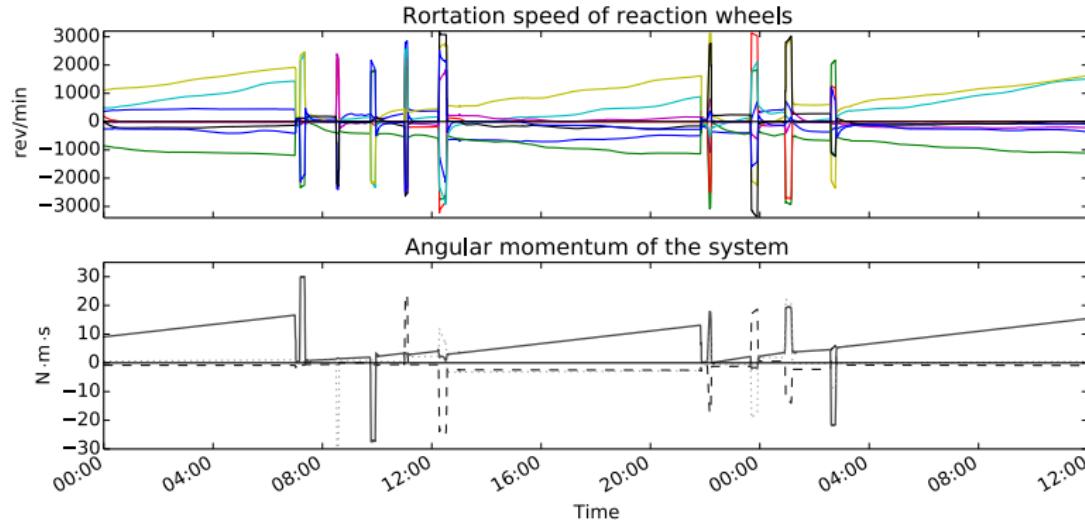
Optical

- CCD RA/Dec: ISON, ASC

Telemetry

- Observed impulses of unloadings $\Delta \mathbf{v}_i^0$.
- Observed torque \mathbf{M} .

Perturbing torque observations



During constant attitude far from the Earth

$$\sum_{i=1}^8 \mathbf{a}_i I_i (\Omega_i(t_2) - \Omega_i(t_1)) = \mathbf{M}_{SRP}(\Lambda, \alpha_1, \mu_1, \alpha_2)(t_2 - t_1).$$

Introduce the following difference of observed and computed torque

$$\zeta = \sum_{i=1}^8 \frac{\mathbf{a}_i I_i [\Omega_i(t_2) - \Omega_i(t_1)]}{t_2 - t_1} - \mathbf{M}_{SRP}(\Lambda, \alpha_1, \mu_1, \alpha_2).$$

Orbit determination

Solve for the following parameters on the interval $[t_b, t_e]$

$$\mathbf{Q} = \{\mathbf{X}_0(t_0), \alpha_1, \mu_1, \alpha_2, \Delta\mathbf{v}_1, \dots, \Delta\mathbf{v}_n\}.$$

using tracking data

$$\Psi = \{\mathbf{D}, \dot{\mathbf{D}}, \dot{\mathbf{D}}_{1w}, \boldsymbol{\alpha}, \boldsymbol{\delta}\}$$

and on-board observations

$$\{\boldsymbol{\Omega}(t), \Delta\mathbf{v}_1^0, \dots, \Delta\mathbf{v}_n^0\}$$

to minimize the functional

$$\begin{aligned}\Phi = & (\Psi_o - \Psi_c)^\top \mathbf{P} (\Psi_o - \Psi_c) + \sum_{j=1}^N \boldsymbol{\zeta}_j^\top \mathbf{P}_j^{sp} \boldsymbol{\zeta}_j + \\ & + \sum_{i=1}^n (\Delta\mathbf{v}_i^0 - \Delta\mathbf{v}_i)^\top \mathbf{P}_i (\Delta\mathbf{v}_i^0 - \Delta\mathbf{v}_i),\end{aligned}$$

Orbit determination

Two intervals have been considered:

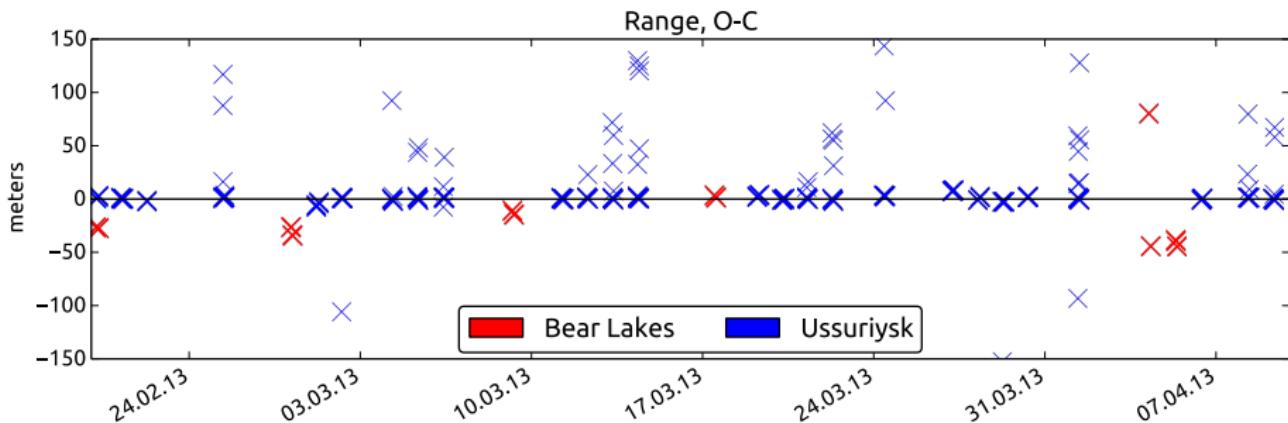
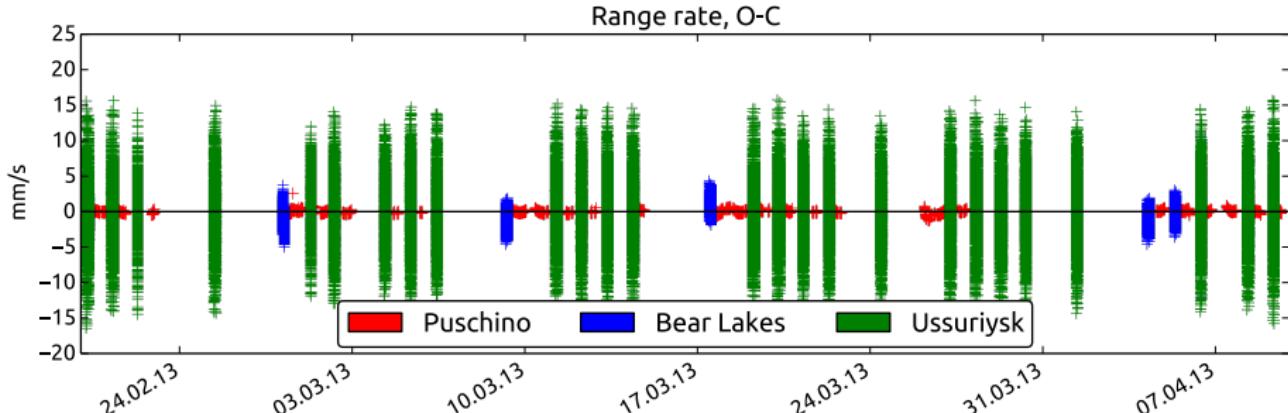
- 20-Feb-2013 – 10-Apr-2013 (Int. 1)
- 10-Apr-2013 – 30-May-2013 (Int. 2)

Several models were used :

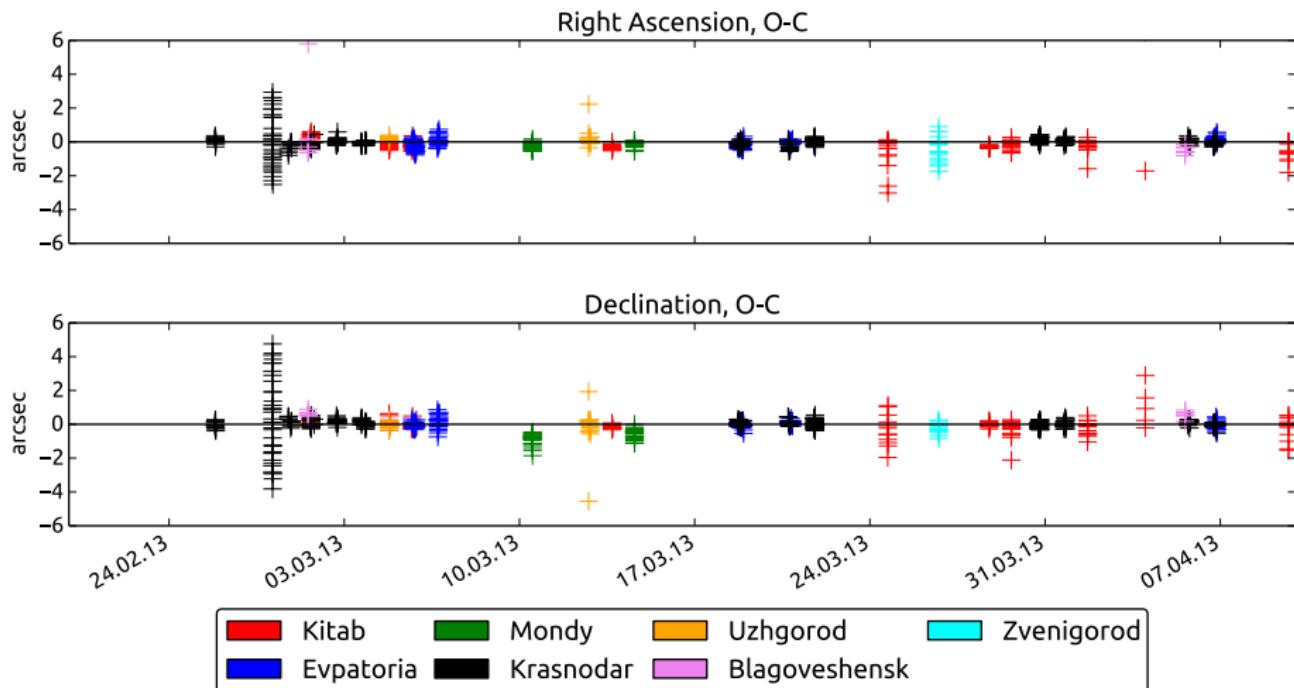
- Simple SRP, No unloadings.
- Simple SRP, unloadings fixed on their nominal values $\Delta\mathbf{v}_i^0$
- SRP depends on three coefficients, unloadings fixed on their nominal values $\Delta\mathbf{v}_i^0$
- SRP depends on three coefficients, unloadings are solved for.

Parameters obtained on the Int. 1 will be used for orbit prediction on the Int. 2.

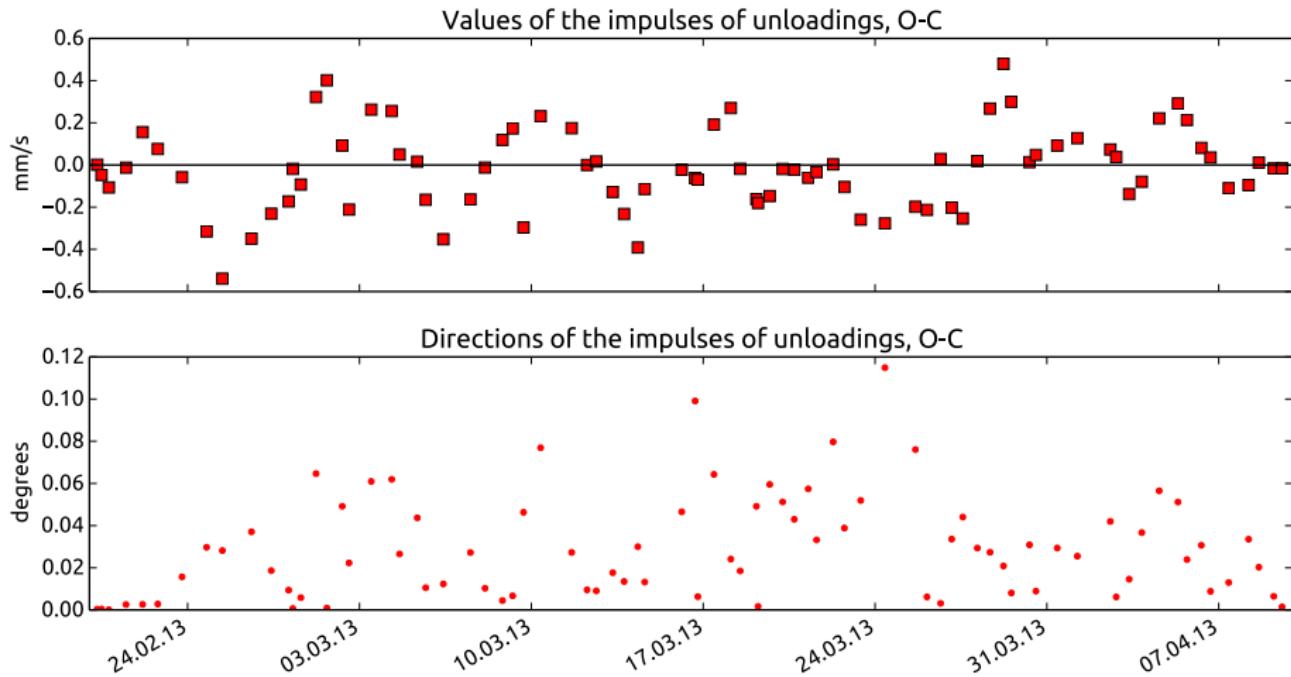
Radioastron D , \dot{D} , 20.02.13 – 10.04.13



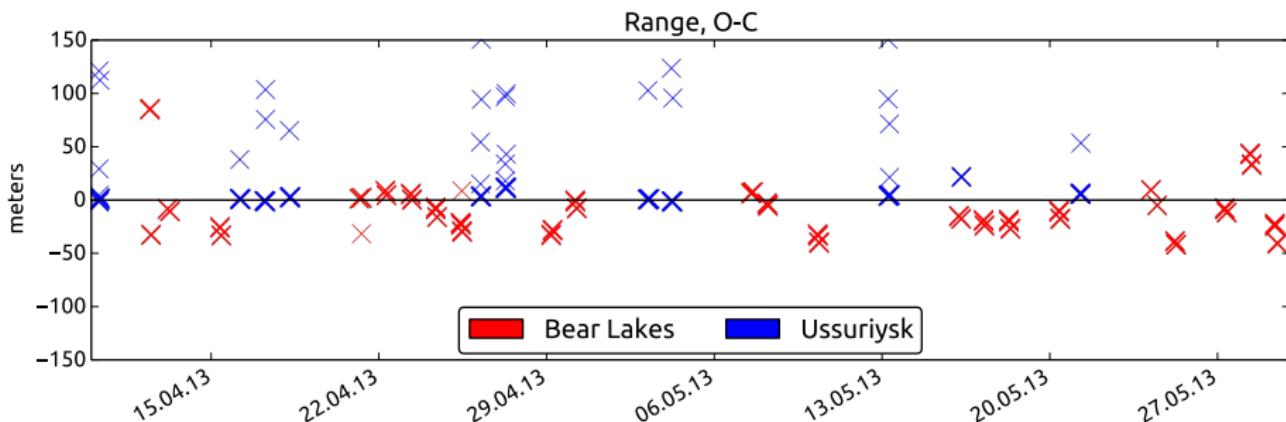
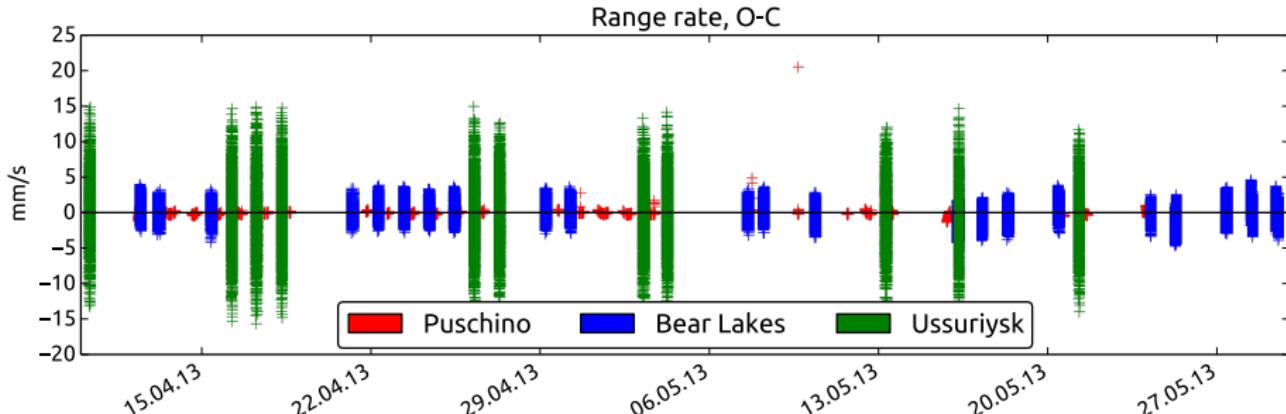
Radioastron (α, δ), 20.02.13 – 10.04.13



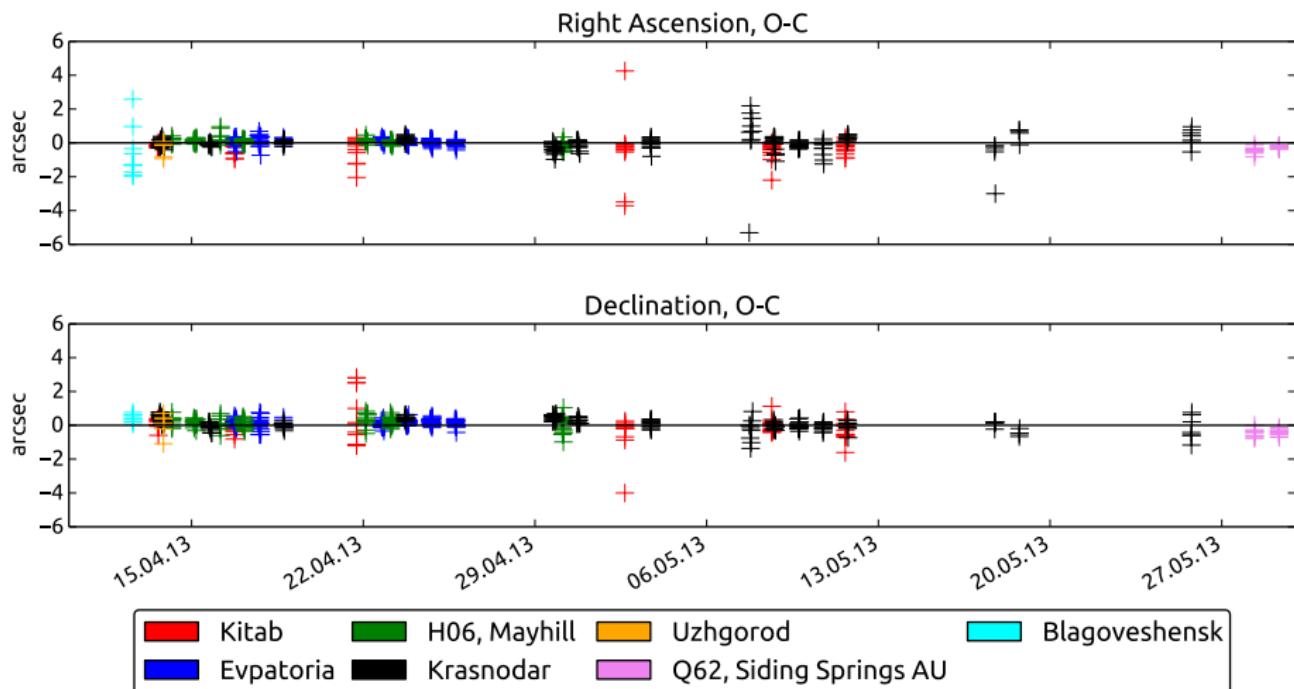
Radioastron $\{\Delta\mathbf{v}_i^0 - \Delta\mathbf{v}_i\}$, 20.02.13 – 10.04.13



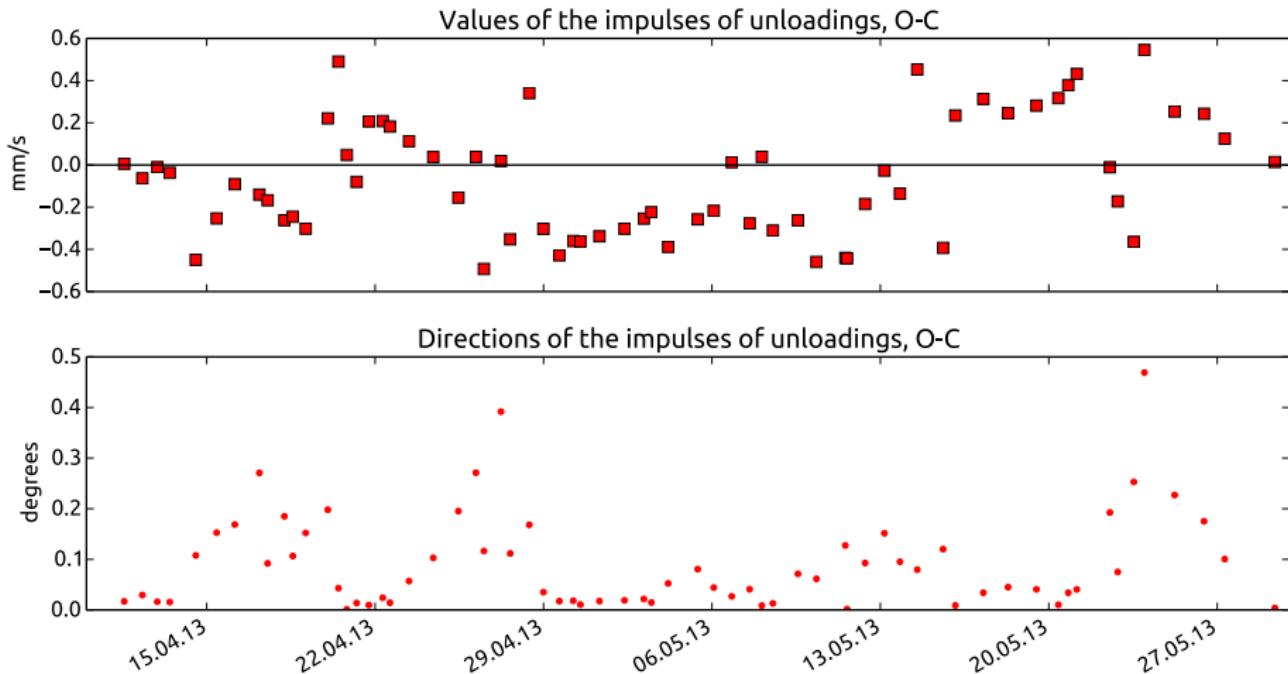
Radioastron D , \dot{D} , 10.04.13 – 30.05.13



Radioastron (α, δ), 10.04.13 – 30.05.13



Radioastron $\{\Delta\mathbf{v}_i^0 - \mathbf{v}_i\}$, 10.04.13 – 30.05.13



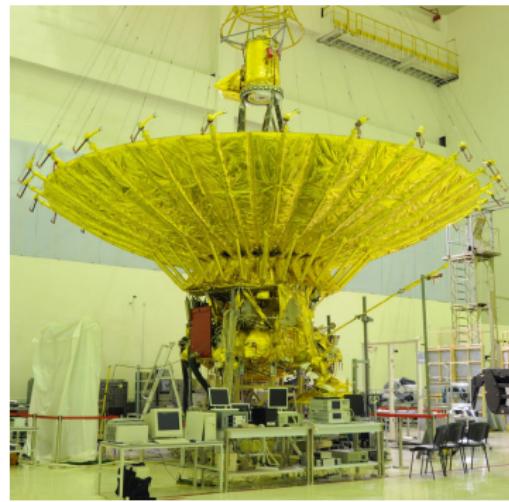
Orbit determination results

Dimensionless standard deviation: 20.02.13 – 10.04.13 (Int. 1) and 10.04.13 – 30.05.13 (Int. 2)

| Nº | SRP model | Unloadings | σ_1 | σ_2 | Δr , km | Δv , mm/s |
|----|--------------------|----------------|------------|------------|-----------------|-------------------|
| 1 | Simple, 1 coeff. | Not considered | 12.43677 | 9.18588 | 71.71 | 288.1 |
| 2 | Simple, 1 coeff. | Nominal | 4.72914 | 6.78832 | 36.76 | 113.3 |
| 3 | Proposed, 3 coeff. | Nominal | 1.20896 | 0.63767 | 7.57 | 8.9 |
| 4 | Proposed, 3 coeff. | Solved for | 0.28198 | 0.24907 | 0.21 | 2.3 |

Estimated solar radiation pressure coefficients

| Parameter | Int. 1 | Int. 2 |
|------------|--------|--------|
| α_1 | 0.754 | 0.791 |
| μ_1 | 0.087 | 0.089 |
| α_2 | 0.063 | 0.102 |



Orbit prediction

Necessary elements

- Attitude forecast (observation schedule + service attitude)

$$(\Lambda_1, t_1, t'_1), (\Lambda_2, t_2, t'_2), \dots (\Lambda_n, t_n, t'_n).$$

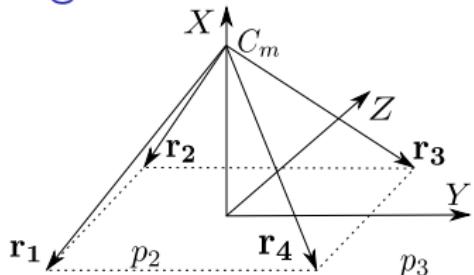
With estimated SRP coefficients determines corresponding perturbation and accumulation of angular momentum by the reaction wheels

- Conversion of accumulated angular momentum to impulses of unloadings

$$\mathbf{K}(t) \xrightarrow{\Delta \mathbf{v}(t)} \mathbf{K}(t + \delta t)$$

- Prediction of times of occurrence of unloadings.

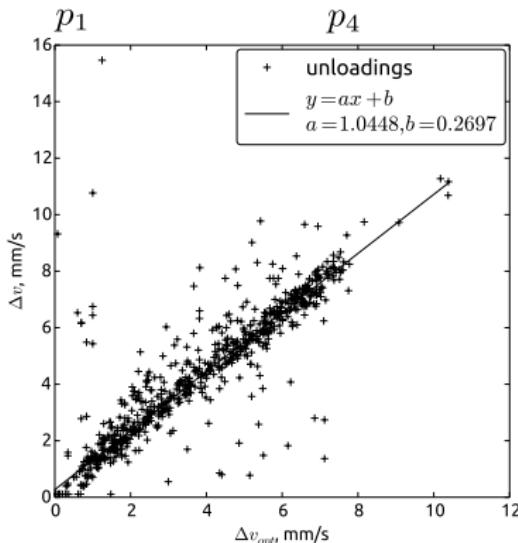
Angular momentum to unloading



Angular momentum changing during an unloading can be described as follows:

$$\sum_{i=1}^8 \mathbf{a}_i I_i \Omega_i(t_u) = \sum_{j=1}^4 \mathbf{r}_j \times \mathbf{e}_j p_j,$$

- an unloading takes relatively short time,
- reaction wheels stop,
- the satellite is not rotating.



where $p_j \geq 0$ are the propellant momenta. The equation can be resolved with respect to $\{p_j\}$ with additional condition:

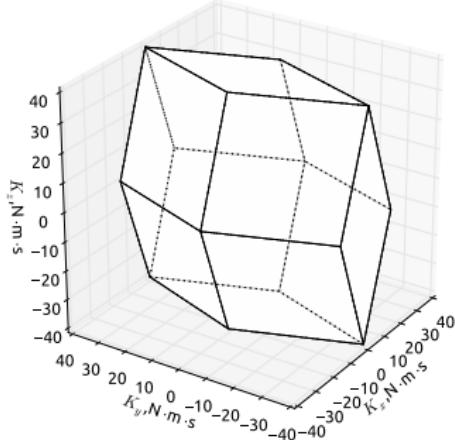
$$\sum_j p_j \rightarrow \min .$$

An impulse of an unloading

$$\Delta \mathbf{v}^*(\mathbf{K}) = -\frac{\sum_i p_i \mathbf{e}_i}{M}, \quad \Delta \mathbf{v} = \Delta \mathbf{v}(\Delta \mathbf{v}^*).$$

Prediction of the time of next unloading

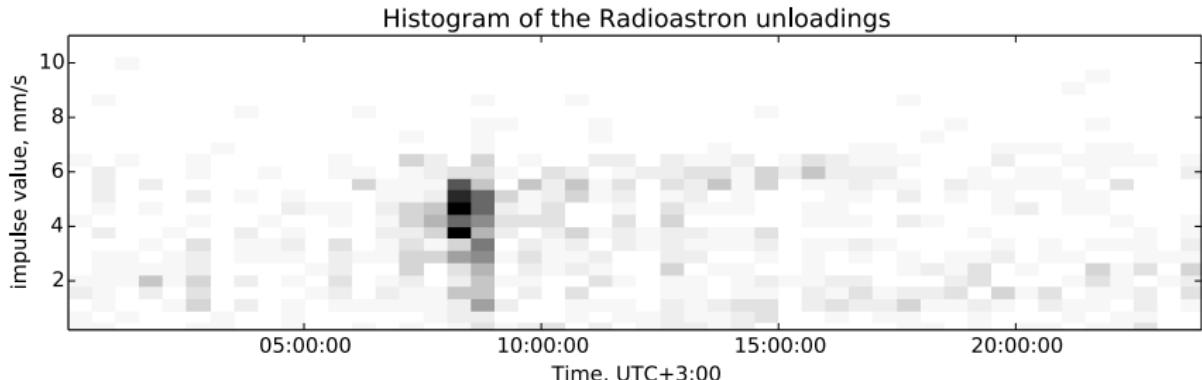
Range of permissible values
of the angular momentum of reaction wheels



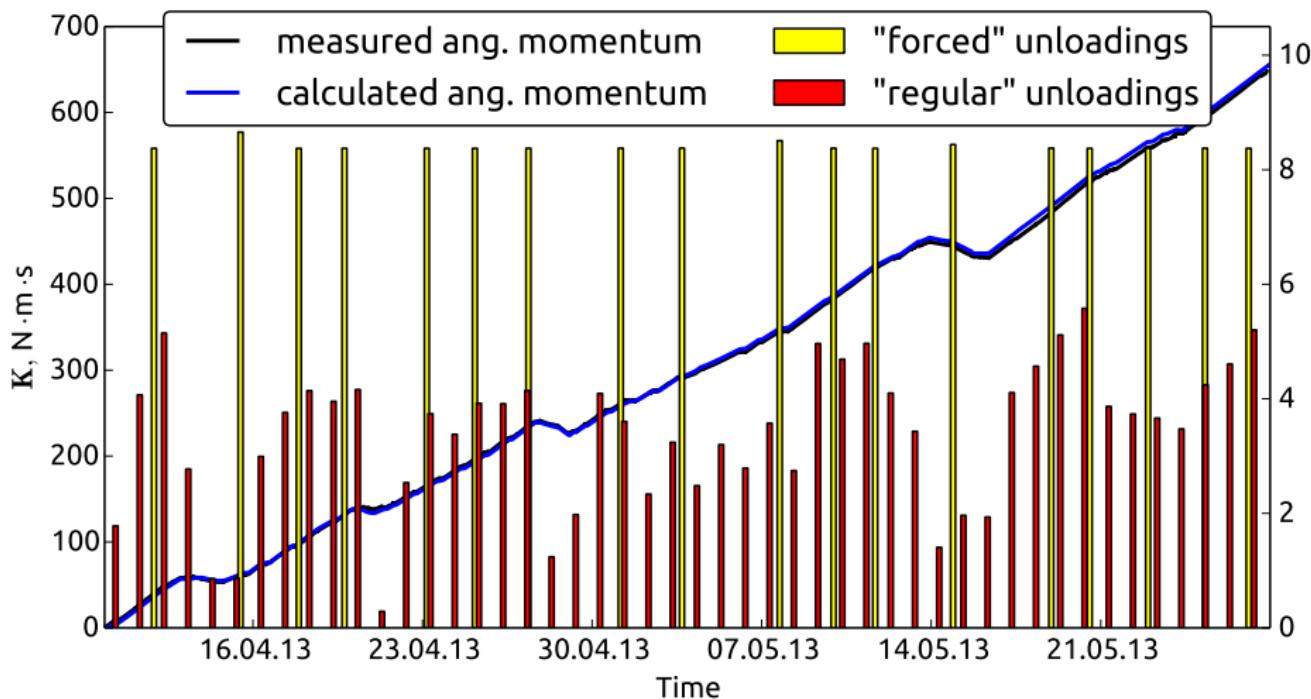
- An unloading should be conducted if accumulated angular momentum is too high $\mathbf{K}(t) \notin U$

$$U = \left\{ \mathbf{K} = \sum_{i=1}^N \mathbf{a}_i I_i \Omega_i : |\Omega_i| \leq \Omega_{max}, i = \overline{1, N} \right\}.$$

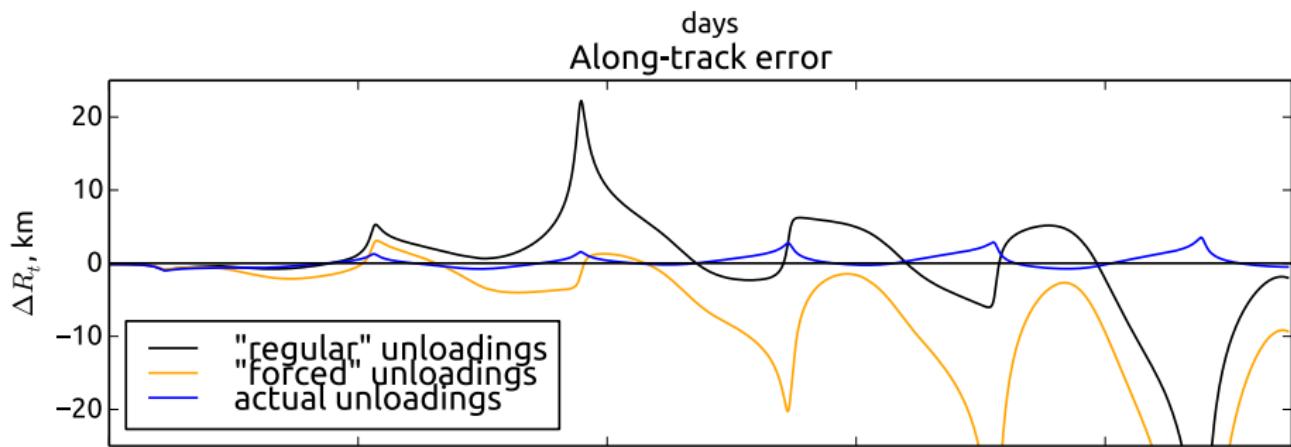
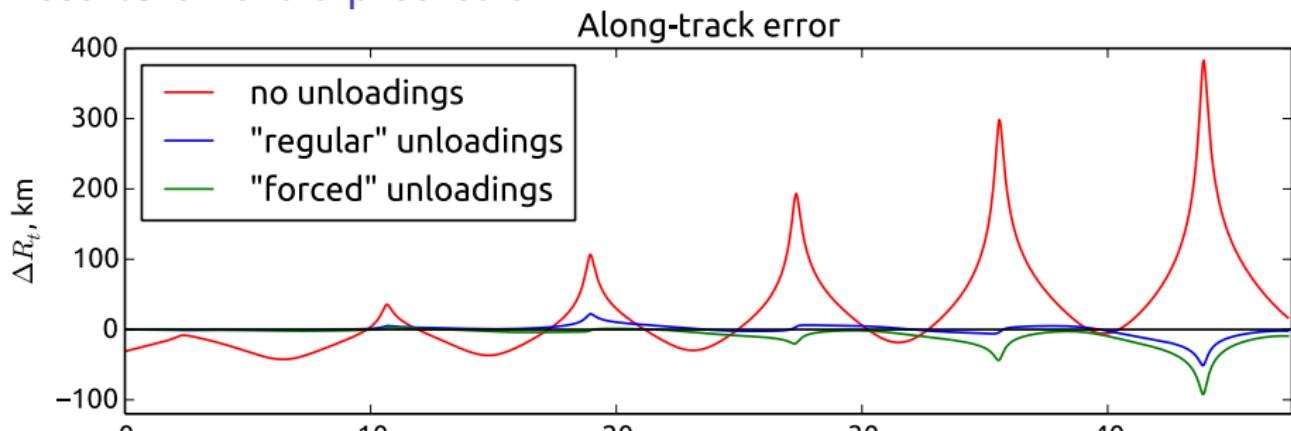
- Unloadings can be conducted on daily basis in the same time



Prediction of unloading on the Int. 2 (10-Apr-2013 – 30-May-2013)



Results of orbit prediction



Summary

- Adjustable Radioastron SRP model was developed and tested.
- Parameters of the SRP model was estimated by using both motion of the center of mass and motion around the center of mass.
- Determined orbits are successfully used for correlation of the Radioastron observations.
- An unloading prediction approach, important for future Sun-Earth L_2 missions (Spectr-R, 'Millimetron') based on the same platform, was tested on the Radioastron data.

Thank you for your attention!